

AN APPROACH TO SIMULTANEOUS SYSTEM DESIGN. PART II: NONSWITCHING GAIN AND DYNAMIC FEEDBACK COMPENSATION BY ALGEBRAIC GEOMETRIC METHODS*

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Abstract. This paper studies structured uncertainty problems in feedback system design, considers a compact parameterization of the space of linear dynamical systems and introduces “base points” and “critical points” as two algebraic-geometric objects that have significance in sensitivity and robustness studies, respectively. Using the Nevanlinna–Pick interpolation theory, the author obtains a necessary and sufficient condition for simultaneous stabilization of a structured one-parameter family of plants. A recent result due to Kharitonov, on the simultaneous stability of a parameterized family of polynomials, leads to a sufficiency condition for simultaneous stabilization of a structured multiparameter family of plants. Furthermore the author considers “simultaneous pole placement” of an r -tuple of plants as a means to arbitrarily tune the natural frequencies of a multimode linear dynamical system. The concept of “nondegenerate” and “twisted” r -tuples of plants is introduced as the pole placement problem is studied via Schubert enumerative geometry as an intersection problem on the associated Grassmannian. Various other design problems, viz., the strong stabilization problem and the dead beat control problem, are also considered.

Key words. simultaneous stabilization, pole assignment, base point, critical point, interpolation, nondegenerate, twisted

AMS(MOS) subject classifications. 93, 14

1. Introduction. In the last decade, control theorists have witnessed significant progress in multi-input multi-output system design. The central issue is the classification of plants or families of plants that admit a robust, nonswitching, dynamic output feedback compensator and satisfy a specific set of design constraints (viz. sensitivity minimization, stabilization, pole assignment, etc.). The basic problem without any additional design restriction is the robust stabilization problem described as follows.

Problem 1.1 (Nonswitching compensator problem). Given a family G of $p \times m$ real, linear dynamical systems, does there exist a nonswitching $m \times p$ real compensator $K(s)$ such that the closed-loop systems $G(s)[I + K(s)G(s)]^{-1}$ have poles only in the open left half of the complex plane for every $G(s) \in G$?

The above problem is important in the design of a compensator for a dynamical system whose parameters are uncertain and where Λ , the region of uncertainty, is known. This would indeed be the case if the parameters of the system were poorly identifiable. In this situation it is important to ascertain the existence of a compensator which is robust with respect to the parameter uncertainty and which stabilizes the family $(G_\lambda(s), \lambda \in \Lambda)$ of plants. Likewise, the above problem would arise if the dynamical system has a continuum of operating points (for example, the altitude of an aircraft or the r.p.m. of an induction motor). The parameters of the system may vary depending upon the choice of the operating points and the objective of the design is to synthesize a compensator robust with respect to the parameter variation. As has been originally pointed out by Saeks and Murray [37], this problem also arises if a control system $G(s)$ operates in many failed modes, all within a given family G , and the design

* Received by the editors September 22, 1986; accepted for publication (in revised form) July 27, 1987. This research was partially supported by the National Aeronautics and Space Administration under grant NSG-2265 while the author was at Harvard University, Cambridge, Massachusetts, and by the National Science Foundation under grant ECS-8414220. This paper is part of the author's Ph.D. thesis at Harvard University.

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objective is to continue to maintain stability even if a component of the control system $G(s)$ should fail. For a detailed discussion concerning many other illustrative examples of the above design problem, we refer the reader to the monograph edited by Ackermann [1], and many other references, e.g., [8]–[10].

We now detail the contribution of this paper. In § 2 we pose Problem 1.1 as a classification or parameterization problem and propose an algebraic geometric framework which enables us to characterize some of the design aspects of the stabilization and pole assignment problem that have not yet been recognized. In particular we compactify the space of dynamic compensators, study the continuity of the pole placement map, and show the existence of “base points.” Finally we argue that the base points are significant, and that, in fact, around these points the location of the closed-loop poles is extremely sensitive with respect to the plant and the compensator parameters. We also study the asymptotic behavior of the closed-loop system as the plant/compensator parameters tend to the base points. We also show the existence of critical points, which are those infinite points in a neighborhood of which the stability of the closed-loop system is not robust with any margin of stability. The principal message of § 2 is therefore to avoid the base points and the critical points in any feedback system design.

In § 3 we describe explicit system design techniques for robust stabilization of a structured family of plants simultaneously. We consider the one-parameter family of plants and, using Nevanlinna–Pick interpolation methods [35], [36], obtain a necessary and sufficient condition for simultaneous stabilization of the family. We also obtain a bound on the degree of the compensator if it exists. Thus whereas the conjecture that “the set of pairs of simultaneously stabilizable plants of bounded degree has simultaneously stabilizing compensators of bounded degree” is false [13], in this paper we show the existence of a suitable class of one-parameter families of simultaneously stabilizable plants of bounded degree that admits simultaneously stabilizing compensators of bounded degree. In other words, the bound on the degree of the compensator can be a priori computed as a function of the degree of the plants to be compensated. In § 3 we also consider the multiparameter family of plants and obtain a sufficiency condition for simultaneous stabilization of such a family. Finally we consider robust simultaneous stabilization problems, wherein we study the extent to which a structured family of simultaneously stabilizable plants can be perturbed by an unstructured perturbation.

In §§ 4 and 5 we describe explicit system design techniques for pole assignment. In § 4 we consider a general ansatz for pole placement as a Schubert intersection problem [19] and derive explicit bounds on the degree of the compensator for generic simultaneous pole placement of proper and strictly proper plants. We also obtain similar bounds for the strong stabilization problem, wherein the dynamic compensator is assumed to be stable. In § 5 we analyze a simultaneous pole assignment problem via gain feedback. We also pose and analyze a classically well-known “dead beat control” problem.

Section 6 concludes this paper with a summary and discussion on future research directions.

2. A parameterization of the space of linear dynamical systems. In this section we consider the set of $m \times p$ proper or strictly proper transfer functions of McMillan degree q denoted, respectively, $S_{p,m}^q$ and $\Sigma_{p,m}^q$. In order to study degenerating families of systems and asymptotic properties of systems under deformation, it is useful to compactify the spaces $\Sigma_{p,m}^q$ and $S_{p,m}^q$ and obtain the spaces $\overline{\Sigma}_{p,m}^q$ and $\overline{S}_{p,m}^q$, respectively.

This construction enables us to study the behavior of a sequence of feedback control systems, in particular the closed-loop poles, as an asymptotic property of a sequence of compensators of a given McMillan degree q . Clearly the above study is useful in system identification, adaptive control and in high gain feedback control system design. It also enables us to study variations in the plant and in the compensator parameters simultaneously arising possibly as a result of parameter changes or structured uncertainty. (For some further details and previous work on families of systems, see [20]-[22], [25], and [32].) The main point that we wish to illustrate in this section is that in every feedback system design problem which involves a family of plants and a family of compensators, there exists a set of points called "base points" in the plant/compensator space which needs to be avoided. Otherwise near the base point the corresponding closed-loop poles are sensitive with respect to changes in the plant and the compensator parameters. Likewise we show that there exists a set of points called "critical points" in the compactified plant/compensator space which cannot be robustly stabilized by a nonswitching regulator.

2.1. A compactification of the space of dynamic compensators. Using a construction due to Hermann and Martin [26], compactification of $S_{p,m}^q$ has been developed by Brockett and Byrnes [3] for $q = 0$ and more recently by Byrnes [4] for $q \geq 0$. Although it is repetitive, we discuss the main results for the sake of completeness. (For a detailed description, see [12].)

To begin with, consider $S_{p,m}^0$ of $m \times p$ gain matrices $-K$. If we consider $-K$ to be a feedback gain matrix, it defines a relation between the m input u and p output y as follows:

$$(2.1.1) \quad [I_m \quad K][u^T \quad y^T]^T = 0.$$

The matrix $[I_m \quad K]$ is an $m \times (m+p)$ matrix with linearly independent rows. In fact, multiplying (2.1.1) by a nonsingular $m \times m$ matrix does not change the relation between u and y . Thus the matrix $[I_m \quad K]$ in fact defines an m -plane in \mathbb{R}^{m+p} via its row span, and is therefore a point in Grass $(m, m+p)$. (See [19] for details about a Grassmannian.)

More generally, consider $S_{p,m}^q$ of $m \times p$ proper transfer functions $K(s)$ of McMillan degree q . If we consider $-K(s)$ to be a feedback compensator, it defines a relation between $u(s)$ and $y(s)$ as follows:

$$(2.1.2) \quad [I_m \quad K(s)][u(s)^T \quad y(s)^T]^T = 0.$$

Let us now consider the left coprime factorization of $K(s)$ given by

$$(2.1.3) \quad K(s) = \begin{bmatrix} k(s) & 0 \\ 0 & k(s) \end{bmatrix}^{-1} \begin{bmatrix} k_{11}(s) & k_{1p}(s) \\ k_{m1}(s) & k_{mp}(s) \end{bmatrix}$$

where $k(s)$, $k_{ij}(s)$, $i = 1, \dots, m$; $j = 1, \dots, p$ are polynomials in s of degree q . Let us write

$$(2.1.4) \quad k(s) \triangleq k^{(0)} + \dots + k^{(q)}s^q,$$

$$(2.1.5) \quad k_{ij}(s) \triangleq k_{ij}^{(0)} + \dots + k_{ij}^{(q)}s^q$$

and define

$$(2.1.6) \quad \underline{k} \triangleq [k^{(0)} \dots k^{(q)}],$$

$$(2.1.7) \quad \underline{k}_{ij} \triangleq [k_{ij}^{(0)} \dots k_{ij}^{(q)}],$$

$$(2.1.8) \quad \underline{u}_i \triangleq [u_i(s), su_i(s), \dots, s^q u_i(s)]^T, \quad i = 1, \dots, m,$$

$$(2.1.9) \quad \underline{y}_j \triangleq [y_j(s), sy_j(s), \dots, s^q y_j(s)]^T, \quad j = 1, \dots, p.$$

We now rewrite (2.1.2) as

$$(2.1.10) \quad \begin{bmatrix} \underline{k} & 0 & \underline{k_{11}} & \cdots & \underline{k_{1p}} \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & \underline{k} & \underline{k_{m1}} & \cdots & \underline{k_{mp}} \end{bmatrix} \begin{bmatrix} u_1 \\ \vdots \\ u_m \\ y_1 \\ \vdots \\ y_p \end{bmatrix} = 0.$$

The associated matrix in (2.1.10) defines (via its row span) an m -plane in $\mathbb{R}^{(q+1)(m+p)}$ and is therefore a point in $\text{Grass}(m, (q+1)(m+p))$. Thus we have

$$(2.1.11) \quad S_{p,m}^q \subset \text{Grass}(m, (q+1)(m+p)).$$

Dually, by considering the right coprime factorization of $K(s)$ in (2.1.3), we also have

$$(2.1.12) \quad S_{p,m}^q \subset \text{Grass}(p, (q+1)(m+p)).$$

The closure $\overline{S_{p,m}^q}$ of $S_{p,m}^q$ inside either $\text{Grass}(m, (q+1)(m+p))$ or $\text{Grass}(p, (q+1)(m+p))$ is compact and is the compactification obtained by Byrnes [4] for $q \geq 0$ and by Brockett and Byrnes [3] for $q = 0$.

DEFINITION 2.1.1. The set of points

$$[\overline{S_{p,m}^q} - S_{p,m}^q]$$

is defined to be the "infinite points" in the above compactification.

Note that the infinite points are the set of limit points which needs to be added to $S_{p,m}^q$ in order to obtain a compact set.

The following example taken from [12] explicitly describes $\overline{S_{2,2}^1}$ in $\text{Grass}(2, 8)$.

Example 2.1.2. Consider the set of two-input and two-output proper systems of degree 1 given by

$$(2.1.13) \quad G(s) = \begin{bmatrix} (a_7s + a_1)/(a_6s + a_5) & (a_8s + a_2)/(a_6s + a_5) \\ (a_9s + a_3)/(a_6s + a_5) & (a_{10}s + a_4)/(a_6s + a_5) \end{bmatrix}$$

where

$$(2.1.14) \quad (a_7a_5 - a_1a_6)(a_8a_5 - a_2a_6) = (a_9a_5 - a_3a_6)(a_{10}a_5 - a_4a_6).$$

The transfer function (2.1.13) defines the point

$$(2.1.15) \quad \text{row span of} \begin{bmatrix} a_5 & a_6 & 0 & 0 & a_1 & a_7 & a_2 & a_8 \\ 0 & 0 & a_5 & a_6 & a_3 & a_9 & a_4 & a_{10} \end{bmatrix}$$

in $\text{Grass}(2, 8)$. Not every element in $\text{Grass}(2, 8)$, however, corresponds to an element in $S_{2,2}^1$ or in $\overline{S_{2,2}^1}$. To see that, consider the point p defined by

$$(2.1.16) \quad p \triangleq \text{row span of} \begin{bmatrix} x_1 & x_2 & x_3 & x_4 & x_5 & x_6 & x_7 & x_8 \\ y_1 & y_2 & y_3 & y_4 & y_5 & y_6 & y_7 & y_8 \end{bmatrix}$$

in $\text{Grass}(2, 8)$. In order that $p \in \overline{S_{2,2}^1}$ it should satisfy

$$(2.1.17) \quad \eta_{12} = \eta_{34} = 0,$$

$$(2.1.18) \quad \eta_{14} = \eta_{23},$$

$$(2.1.19) \quad \eta_{13}\eta_{68} + \eta_{24}\eta_{57} + \eta_{23}[\eta_{58} + \eta_{67}] = 0,$$

$$(2.1.20) \quad \eta_{24} \neq 0,$$

and

$$(2.1.21) \quad (\eta_{24}\eta_{54} \neq \eta_{14}\eta_{64} \text{ or } \eta_{24}\eta_{74} \neq \eta_{14}\eta_{84} \text{ or } \eta_{24}\eta_{25} \neq \eta_{14}\eta_{26} \text{ or } \eta_{24}\eta_{27} \neq \eta_{14}\eta_{28})$$

where $\eta_{ii} = x_i y_i - x_i' y_i'$ is the set of Plucker coordinates (see [7]) via which Grass (2, 8) can be imbedded in \mathbb{RP}^{27} . Note that the infinite points in $\overline{S_{2,2}^1}$ are described by (2.1.17)-(2.1.19) and

$$(2.1.22) \quad \eta_{24} = 0$$

or

$$(2.1.23) \quad \frac{\eta_{24}}{\eta_{14}} = \frac{\eta_{64}}{\eta_{54}} = \frac{\eta_{84}}{\eta_{74}} = \frac{\eta_{26}}{\eta_{25}} = \frac{\eta_{28}}{\eta_{27}}.$$

We remark that (2.1.17)-(2.1.19) and (2.1.22) contain the set of improper transfer functions in $\overline{S_{2,2}^1}$, and that (2.1.17)-(2.1.19) and (2.1.23) describe the set of transfer functions of degree 0 in $\overline{S_{2,2}^1}$.

By analogous technique we can compactify $\Sigma_{p,m}^q$, the set of $m \times p$ strictly proper transfer functions of degree q as a point in Grass ($m, (q+1)m + qp$) or Grass ($p, (q+1)p + qm$). Let us now consider the following example.

Example 2.1.3. Consider the set $\Sigma_{2,2}^1$ given by (2.1.13), (2.1.14) with $a_7 = a_8 = a_9 = a_{10} = 0$. Every transfer function in $\Sigma_{2,2}^1$ defines a point in Grass (2, 6) given by

$$(2.1.24) \quad \text{row span of } \begin{bmatrix} a_5 & a_6 & 0 & 0 & a_1 & a_2 \\ 0 & 0 & a_5 & a_6 & a_3 & a_4 \end{bmatrix}.$$

In fact if p is a point in Grass (2, 6) defined by

$$(2.1.25) \quad \text{row span of } \begin{bmatrix} x_1 & x_2 & x_3 & x_4 & x_5 & x_6 \\ y_1 & y_2 & y_3 & y_4 & y_5 & y_6 \end{bmatrix},$$

then $p \in \Sigma_{2,2}^1$ if and only if

$$(2.1.26) \quad \eta_{12} = \eta_{34} = 0, \quad \eta_{14} = \eta_{23}, \quad \eta_{56} = 0, \quad \eta_{24} \neq 0.$$

It follows that $\overline{\Sigma_{2,2}^1} - \Sigma_{2,2}^1$ is described by

$$(2.1.27) \quad \eta_{12} = \eta_{34} = \eta_{56} = \eta_{24} = 0, \quad \eta_{14} = \eta_{23} = 0.$$

2.2. Continuity of the pole placement map and the base locus condition. Classically, root locus [11] was studied by considering a single-input single-output plant together with a scalar gain feedback, and a plot of the closed-loop poles as a function of the feedback gain was obtained. Since root locus is continuous with respect to the scalar gain, the closed-loop poles asymptotically and continuously approach the open-loop zeros as the gain tends to infinity. For the multi-input multi-output case the generalization is not immediate. However, as we shall see in this section, the asymptotic locus of the closed-loop poles as a function of the compensator parameters is not necessarily continuous. Furthermore, as we have seen in § 2.1, infinity is not a single point and therefore there is more than one way to tend to infinity leading to distinct closed-loop behavior of the dynamical system. These are now detailed as follows.

Let $G(s)$ be a proper $p \times m$ plant of McMillan degree n and let $K(s)$ be a proper $m \times p$ compensator of McMillan degree q . Let us represent them in their coprime fraction representation as follows:

$$(2.2.1) \quad G(s) = N_p(s) D_p(s)^{-1},$$

$$(2.2.2) \quad K(s) = D_c(s)^{-1} N_c(s)$$

where $N_p(s)$, $D_p(s)$, $N_c(s)$, $D_c(s)$ are matrices of appropriate orders with elements in the ring H of stable proper rational functions. It is well known that $K(s)$ places the poles of the plant $G(s)$ at $s = s_1, s_2, \dots, s_{n+q}$ provided

$$(2.2.3) \quad \det [N_c(s)N_p(s) + D_c(s)D_p(s)](s_i) = 0$$

for $i = 1, \dots, n+q$. Let

$$(2.2.4) \quad c_0 + c_1s + \dots + c_{n+q}s^{n+q} \triangleq p(s)$$

be a polynomial which vanishes precisely where $\det [N_cN_p + D_cD_p]$ vanishes. The polynomial $p(s)$ is called the characteristic polynomial. For a fixed $G(s)$, (2.2.3) defines a mapping between the compensator parameters and the coefficients c_i of the characteristic polynomial $p(s)$ in (2.2.4). We therefore define the pole placement map

$$(2.2.5) \quad \chi: \overline{S_{p,m}^q} - B \rightarrow \mathbb{R}\mathbb{P}^{n+q}$$

defined by

$$(2.2.6) \quad \chi(K(s)) = [c_0, \dots, c_{n+q}]$$

where the right-hand side of (2.2.6) is written in homogeneous coordinates. The set B is called the base locus (see [19], [34]) and is defined to be the set of points in $\overline{S_{p,m}^q}$, where χ does not have a continuous extension. It is a well-known fact (see [34, p. 98]) that the base locus B is given by

$$(2.2.7) \quad B \triangleq \bigcap_H \overline{\chi^{-1}(H)}$$

where H is a hyperplane in $\mathbb{R}\mathbb{P}^{n+q}$ and $\overline{\chi^{-1}(H)}$ is the closure of $\chi^{-1}(H)$ inside $\overline{S_{p,m}^q}$. The significance of the base locus is made clear in the following proposition.

PROPOSITION 2.2.1. *The base locus B is equivalently described as*

$$(2.2.8) \quad B = \{K(s) \mid \det [N_c(s)N_p(s) + D_c(s)D_p(s)] \equiv 0\}.$$

Proof. Every $s_i \in \mathbb{R}$ defines a hyperplane H_i in $\mathbb{R}\mathbb{P}^{n+q}$, viz., the hyperplane orthogonal to the vector $[1 \ s_i \ s_i^2 \ \dots \ s_i^{n+q}]$. It follows that

$$(2.2.9) \quad \overline{\chi^{-1}(H_i)} = \{K(s) \mid \det [N_cN_p + D_cD_p](s_i) = 0\}.$$

Let s_1, \dots, s_{n+q+1} be a set of distinct real numbers. It follows that

$$(2.2.10) \quad \bigcap_{i=1}^{n+q+1} \overline{\chi^{-1}(H_i)} = \{K(s) \mid \det [N_cN_p + D_cD_p](s) \equiv 0\},$$

since the characteristic polynomial of the closed-loop transfer function is of degree $n+q$. Finally since

$$(2.2.11) \quad B \subset \bigcap_{i=1}^{n+q+1} \overline{\chi^{-1}(H_i)},$$

we have

$$(2.2.12) \quad B \subset \{K(s) \mid \det [N_c(s)N_p(s) + D_c(s)D_p(s)] \equiv 0\}.$$

Conversely, let us assume that

$$(2.2.13) \quad K_1(s) \in \{K(s) \mid \det [N_c(s)N_p(s) + D_c(s)D_p(s)] \equiv 0\}.$$

Clearly $K_1(s)$ is a compensator for which the associated characteristic polynomial $p(s)$ is identically zero, i.e., $c_0 = c_1 = \dots = c_{n+q} = 0$. Hence χ cannot be defined at $K_1(s)$. By choosing two different sequences of compensators approaching $K_1(s)$, we can show

that χ does not even have a continuous extension to a mapping which is defined at $K_1(s)$. Otherwise χ has to be multivalued at $K_1(s)$, which is absurd. Therefore

$$(2.2.14) \quad \{K(s) | \det [N_c(s)N_p(s) + D_c(s)D_p(s)] \equiv 0\} \subset B. \quad \square$$

In the following example we characterize the base locus for a particular compensation problem.

Example 2.2.2. Consider a single-input single-output plant $g(s)$ of degree 1 given by $(s+1)/(s+2)$. Consider a proper compensator $k(s)$ of degree 1 given by $(k_1s-2)/(s+k_2)$. The compensator is parameterized by two parameters k_1 and k_2 . The closed-loop transfer function is given by

$$(2.2.15) \quad \frac{(s+1)(s+k_2)}{(k_1+1)s^2 + (k_1+k_2)s + (2k_2-2)}.$$

Using Proposition 2.2.1 we infer that the base locus B is the point set given by

$$(2.2.16) \quad B \triangleq \{k(s) | k_1 = -1, k_2 = 1\}.$$

The pole placement map χ is described as

$$(2.2.17) \quad \chi: S_{1,1}^1 - B \rightarrow \mathbb{R}P^2,$$

$$(2.2.18) \quad \chi(k(s)) = \{k_1 + 1, k_1 + k_2, 2k_2 - 2\}.$$

Clearly χ is continuous everywhere except at $k(s) = -(s+2)/(s+1)$ where it is not even defined. To show that χ cannot be extended to a function χ_1 continuous at $-(s+2)/(s+1)$, we assume the parameterized family of compensators F_t given by

$$(2.2.19) \quad F_t \triangleq \{k(s) | (k_1 + 1) = t(k_2 - 1)\}$$

where $t \in \mathbb{R}$. Consider a sequence of compensators $h_1^{(i)}(s), h_2^{(i)}(s), \dots$ in F_t approaching the compensator $-(s+2)/(s+1)$. It is easy to see that

$$(2.2.20) \quad \chi(h_i^{(i)}(s)) = [t \quad (t+1) \quad 2]$$

independent of i but dependent on t . Note that the closed-loop system is stable if $t > 0$ and unstable otherwise. This indicates that when the compensator parameters k_1, k_2 approach arbitrarily close to the point $(-1, 1)$, possibly along two different lines in the (k_1, k_2) plane, the closed-loop system can be stable in one case and unstable in the other. Thus stability is not a robust property in the neighborhood of $(-1, 1)$ primarily because the closed-loop poles are extremely sensitive with respect to the parameter t . Finally the asymptotic locus of the roots of the characteristic polynomial is not continuous with respect to the parameters k_1, k_2 at the point $(-1, 1)$. Hence χ does not have a continuous extension to a function χ_1 defined at the point $(-1, 1)$.

2.3. Degeneration of a family of closed-loop systems. In the last section we derived the base locus condition assuming that the plant is fixed and the compensator parameters are allowed to vary. In this section we describe a general theory, wherein both the plant and the compensator parameters are allowed to vary. Let us consider the set $\overline{S_{m,p}^n}$ of $p \times m$ plants of degree n and the set $\overline{S_{p,m}^q}$ of $m \times p$ compensators of degree q suitably compactified. As an extension of the pole placement map (2.2.5) we define

$$(2.3.1) \quad \psi: \overline{S_{m,p}^n} \times \overline{S_{p,m}^q} - \tilde{B} \rightarrow \mathbb{R}P^{n+q},$$

$$(2.3.2) \quad \psi(G(s), K(s)) = [c_0, \dots, c_{n+q}]$$

where $G(s)$, $K(s)$, c_i , $i=0, \dots, n+q$ are described via (2.2.1)–(2.2.4). Similar to the definition of B , we define \tilde{B} to be the base locus of the map ψ . We now consider the following proposition.

PROPOSITION 2.3.1. *The base locus \tilde{B} is described as*

$$(2.3.3) \quad \tilde{B} = \{(G(s), K(s)) \mid \sigma[N_c(s)N_p(s) + D_c(s)D_p(s)] = 0 \forall s \in \mathbb{C} \\ \text{where } \sigma(\cdot) \text{ denotes the minimum singular value}\}.$$

Proof. The proof follows from Proposition 2.2.1 since

$$(2.3.4) \quad \sigma[N_c(s)N_p(s) + D_c(s)D_p(s)] = 0 \quad \text{for all } s \in \mathbb{C},$$

$$(2.3.5) \quad \Leftrightarrow \det[N_c(s)N_p(s) + D_c(s)D_p(s)] \equiv 0. \quad \square$$

We now consider the following illustrative example from the literature [33, Ex. 2.1], wherein the compensator is fixed and the plant parameters degenerate into the base locus.

Example 2.3.2. Assume $b_{12} \neq 0$. Consider the following state-space system:

$$(2.3.6) \quad \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 & b_{12} \\ 0 & 1 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix},$$

$$(2.3.7) \quad [y_1^T \quad y_2^T]^T = [x_1^T \quad x_2^T]^T$$

together with the feedback compensator

$$(2.3.8) \quad [u_1^T \quad u_2^T]^T = -[y_1^T \quad y_2^T]^T.$$

The closed-loop system above is stable and has a pair of poles at $-2, -2$. Let us now perturb (2.3.6) and consider

$$(2.3.9) \quad \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 & b_{12} \\ 5/b_{12} & 1 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}.$$

The perturbed system (2.3.9), (2.3.7), (2.3.8) is an unstable system with closed-loop poles at the zeros of $(s+2)^2 - 5$. Note that the stability of the closed-loop system and the instability of the perturbed closed-loop system are independent of b_{12} . This fact is quite disturbing because, for arbitrary large b_{12} , the matrix components of the two systems are “close.”

From the viewpoint of the parameterization proposed in § 2.1, it may be trivially checked that the unperturbed system defines a point in Grass $(2, 8)$ given by

$$(2.3.10) \quad \text{row span of } \begin{bmatrix} 1 & 1 & 0 & 0 & 1 & 0 & b_{12} & 0 \\ 0 & 0 & 1 & 1 & 0 & 0 & 1 & 0 \end{bmatrix}$$

which degenerates to the point

$$(2.3.11) \quad \text{row span of } \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 1 & 1 & 0 & 0 & 0 & 0 \end{bmatrix}$$

as $b_{12} \rightarrow \infty$. The perturbed system, on the other hand, defines the point

$$(2.3.12) \quad \text{row span of } \begin{bmatrix} 1 & 1 & 0 & 0 & 1 & 0 & b_{12} & 0 \\ 0 & 0 & b_{12} & b_{12} & 5 & 0 & 1 & 0 \end{bmatrix}$$

which also degenerates to the point (2.3.11) as $b_{12} \rightarrow \infty$. Thus the two closed-loop systems under consideration are “close” as points on Grass $(2, 8)$.

It may be trivially checked that the point (2.3.11) is on the base locus of the map

$$(2.3.13) \quad \psi: \overline{S_{2,2}^2} \times \overline{S_{2,2}^0} - \tilde{B} \rightarrow \mathbb{R}P^2.$$

Thus, following the argument presented in Example 2.2.2, we conclude that stability is not a robust property around the point (2.3.11). This may also be viewed as an algebraic-geometric interpretation of the conclusion presented in Example 2.1 of [33].

Remark 2.3.3. Proposition 2.3.1 serves to justify the comment on page 78 of [33]: "A multivariable system will not be robust . . . if its return difference transfer function matrix . . . is nearly singular at some frequency . . ." In fact, a near singular transfer function matrix is close to the base locus.

In multivariable feedback system design, a good design strategy is to avoid the base locus. In particular, around the base locus, the closed-loop poles are sensitive with respect to the plant and the compensator parameters. (For an original reference on the application of base locus in system theory, see Byrnes [45].)

2.4. Robust system design and the critical point condition. Let $\overline{S_{p,m}^q}$ be as defined in § 2.1. For the purpose of robust system design, in this section we pose the following problem.

Problem 2.4.1. Parameterize the set $\Omega_{p,m}^q$ of points in $\overline{S_{p,m}^q}$ with the property that for every $\sigma \in \Omega_{p,m}^q$ there exists an open neighborhood $N(\sigma)$ of σ in $\overline{S_{p,m}^q}$ such that every plant in $S_{p,m}^q \cap N(\sigma)$ is simultaneously stabilizable.

Analysis of the above problem is clearly important in the study of "system degeneration" and "high gain" compensation. (For motivational remarks and other details pertaining to the case $m = p = 1$, see [6].)

DEFINITION 2.4.2. The set of points

$$(2.4.1) \quad \overline{S_{p,m}^q} - \Omega_{p,m}^q$$

is defined as the "critical points" in the compactified $\overline{S_{p,m}^q}$.

We now state the following simple proposition.

PROPOSITION 2.4.3. Every critical point is an infinite point in $\overline{S_{p,m}^q}$.

Proof. The finite points in $\overline{S_{p,m}^q}$ are points in $S_{p,m}^q$. Moreover, every point in $S_{p,m}^q$ has an open neighborhood in $S_{p,m}^q$ that can be simultaneously stabilized by a dynamic compensator. Therefore no point in $S_{p,m}^q$ is a critical point. \square

The set of critical points are now explicitly characterized as follows.

THEOREM 2.4.4. The points

$$(2.4.2) \quad \text{row span of } \begin{bmatrix} k & 0 & | & k_{11} & k_{12} & \cdots & k_{1p} \\ \vdots & \vdots & | & \vdots & \vdots & \ddots & \vdots \\ 0 & k & | & k_{m1} & k_{m2} & \cdots & k_{mp} \end{bmatrix}$$

belonging to $\overline{S_{p,m}^q}$ are critical points of $\overline{S_{p,m}^q}$ if and only if there exists s^* in the closed right half of the complex plane such that the row rank of the matrix $M(s)$ given by

$$(2.4.3) \quad M(s) \triangleq \begin{bmatrix} k(s) & 0 & | & k_{11}(s) & \cdots & k_{1p}(s) \\ \vdots & \vdots & | & \vdots & \ddots & \vdots \\ 0 & k(s) & | & k_{m1}(s) & \cdots & k_{mp}(s) \end{bmatrix}$$

at $s = s^*$ is $< m$.

Remark 2.4.5. The vectors k, k_i and the polynomials $k(s), k_i(s), i = 1, \dots, m; j = 1, \dots, p$ are defined in (2.1.4)-(2.1.7).

Proof of Theorem 2.4.4. The sufficiency is clear, since the closed-loop characteristic polynomial

$$(2.4.4) \quad \det \left[\begin{array}{ccc|ccc} k(s) & & 0 & k_{11}(s) & \cdots & k_{1p}(s) \\ & \ddots & & \vdots & & \vdots \\ 0 & & k(s) & k_{m1}(s) & \cdots & k_{mp}(s) \\ \hline & & K(s) & & & I \end{array} \right]$$

corresponding to any $p \times m$ compensator transfer function $K(s)$ always vanishes at s^* and therefore (2.4.2) is indeed a critical point.

In order to show "necessity" assume that the row rank of the matrix $M(s)$ in (2.4.3) is m for all $s \in \mathbb{C}$. Then clearly $M(s)$ is right invertible, i.e., there exists an $(m+p) \times m$ matrix $N(s)$ | $M(s)N(s) = \Delta(s)$, where $\det \Delta(s)$ vanishes only in \mathbb{C}_s , the open left half of the complex plane. We partition $N(s)$ as $[N_1(s)^T \ N_2(s)^T]^T$, where $N_1(s)$ is $m \times m$ and where we choose $N(s)$ such that $\det N_1(s) \neq 0$ and $N_1^{-1}N_2$ is proper. Thus we have a transfer function $N_1^{-1}N_2$ of a compensator which stabilizes the transfer function corresponding to the plant (2.4.2). Moreover, a sufficiently small neighborhood of (2.4.2) in $S_{p,m}^q$ is stabilized by the compensator. It follows that (2.4.2) is not a critical point. The only case left is that where the rank of the matrix $M(s)$ in (2.4.3) is $< m$ at some points in \mathbb{C}_s , the open left half of the complex plane. This fact, however, implies that $M(s)$ can be factored as

$$(2.4.5) \quad M(s) = \Delta_1(s)M_1(s)$$

where $\det \Delta_1(s)$ vanishes at $s = s_1$ and where $M_1(s)$ has either rank m at all $s \in \mathbb{C}_s$ or rank $< m$ for some $s = s_2$ in \mathbb{C}_s . Proceeding as above it follows that $M(s)$ can be factored as

$$(2.4.6) \quad M(s) = \Delta^*(s)M^*(s)$$

where $\det \Delta^*(s)$ vanishes only in \mathbb{C}_s and where $M^*(s)$ is of rank m at all $s \in \mathbb{C}$. By obtaining a right inversion of $M^*(s)$ and considering the reasoning as before it follows that (2.4.2) is not a critical point. \square

Example 2.4.6. If $q = m = p = 1$, the space $S_{1,1}^1$ contains proper transfer functions

$$(2.4.7) \quad q(s) = \frac{a_1s + a_0}{s + b_0}, \quad a_0 \neq a_1b_0$$

of degree 1, that can be parameterized as points in \mathbb{RP}^3 via the homogeneous coordinates $[1 \ b_0 \ a_1 \ a_0]$. The set of infinite points $\overline{S_{1,1}^1} - S_{1,1}^1$ in \mathbb{RP}^3 is described as

$$(2.4.8) \quad \{[h_0, h_1, h_2, h_3]: h_0h_3 = h_1h_2\}$$

and the set of critical points are described as

$$(2.4.9) \quad \{[h_0, h_1, h_2, h_3]: h_0h_3 = h_1h_2 \text{ and } h_0h_1 \leq 0 \text{ and } h_2h_3 \leq 0\}.$$

Remark 2.4.7. The significance of a critical point may now be emphasized. By definition, if ξ is a critical point in $\overline{S_{p,m}^q}$, then there exists a sequence of points $\xi_i, i = 1, 2, \dots$, in $S_{p,m}^q$ which tends to ξ in the limit and with the property that the family of plants $\{\xi_i\}$ is simultaneously unstabilizable by a dynamic compensator. Since critical points are those infinite points in $\overline{S_{p,m}^q}$, neighborhoods of which are not simultaneously stabilizable, a good design strategy is to avoid the critical points in system design.

In order to describe Corollary 2.4.9 of Theorem 2.4.4 we need the following definition.

DEFINITION 2.4.8. A compensator is said to stabilize a plant with margin of stability $\varepsilon > 0$ if the closed-loop poles are in the region $\{s \in \mathbb{C}: \operatorname{Re} s < -\varepsilon\}$.

COROLLARY 2.4.9. Let $\xi_1(s), \xi_2(s), \dots$ be a sequence of plants in $S_{p,m}^q$ which approaches a critical point in $\overline{S_{p,m}^q} - \Omega_{p,m}^q$ arbitrarily close. Then the family $\{\xi_i(s), i = 1, 2, \dots\}$ of plants is not simultaneously stabilizable with any margin of stability.

Proof. Suppose the corollary does not hold. Then there exists a compensator which simultaneously stabilizes the given family with a margin of stability $\varepsilon > 0$. This, however, implies that the plants $\xi_i(s)$ in the family are not in the associated base locus. Thus the closed-loop poles are continuous with respect to the plant parameters. It follows from the definition of a critical point that there exists an integer N sufficiently large that $\xi_N(s)$ has a closed-loop pole arbitrarily close to a point s^* in the closed right half of the complex plane. However, this is a contradiction. \square

3. Simultaneous stabilization of plants with structured uncertainty. In this section we restrict our attention to single-input single-output plants and consider the following problem.

Problem 3.1. Let P be a subset of $\Omega_{1,1}^n$ for some integer n . Does there exist a dynamic compensator of degree $\leq q$ which stabilizes each and every plant $\sigma \in P$?

Of course if σ_0 is a plant in P and if the subset P represents structured perturbation of σ_0 in $\Omega_{1,1}^n$, the above Problem 3.1 is a robust stabilization problem with structured uncertainty. Also, for the purpose of estimating the complexity of the compensator which solves a particular design problem, it is of interest to consider.

Question 3.2. Is q a priori bounded?

If P is a single point it is well known that an upper bound on q is given by $q \leq n$. On the other hand it has been shown [13], [12] that if P is a pair of points in $\Omega_{1,1}^n$, an upper bound on q does not exist.

3.1. A general ansatz for simultaneous stabilization. In this section, we consider a family P of single-input single-output proper plants of degree n given by

$$(3.1.1) \quad P = \{x_\lambda(s)/y_\lambda(s): \lambda \in \Lambda, x_\lambda, y_\lambda \in H; x_\lambda, y_\lambda \text{ are coprime and } \deg x_\lambda/y_\lambda = n \text{ for all } \lambda \in \Lambda\}.$$

Assume that P contains at least two distinct plants. Furthermore let us define

$$(3.1.2) \quad \eta_{ij}(s) = x_i(s)y_j(s) - x_j(s)y_i(s), \quad i, j \in \Lambda$$

where Λ is an arbitrary parameter space. We now state without proof the following result from Theorem 5.1 of [13].

PROPOSITION 3.1.1. Let $x_1(s)/y_1(s), x_2(s)/y_2(s)$ be two distinct plants in P . There exists a proper compensator which simultaneously stabilizes each and every plant in P if and only if there exist $\Delta_1(s), \Delta_2(s) \in J$, the set of multiplicative units of H , such that

(i) $\Delta_1 y_2 - \Delta_2 y_1$ and $\Delta_2 x_1 - \Delta_1 x_2$ vanish at $s_1, \dots, s_r \in \mathbb{C}_u$ with multiplicities at least m_1, \dots, m_r , respectively, where s_1, \dots, s_r are the zeros of $\eta_{12}(s)$ in \mathbb{C}_u with multiplicities m_1, \dots, m_r , respectively. (Here $\mathbb{C}_u = \mathbb{C} - \mathbb{C}_\infty$.)

(ii) $\Delta_2 x_1 - \Delta_1 x_2$ does not vanish at ∞ with multiplicity m_∞ unless $\eta_{12}(s)$ vanishes at ∞ with multiplicity at least m_∞ .

(iii) There exists $\Delta_\lambda \in J$ for all $\lambda \in \Lambda - \{1, 2\}$ such that

$$(3.1.3) \quad \Delta_1 \eta_{\lambda 2} - \Delta_2 \eta_{\lambda 1} = \Delta_\lambda \eta_{12}.$$

In the proof of the next theorem we will introduce four auxiliary return difference polynomials which we denote by $\alpha_i(s), i = 1, 2, 3, 4$.

Let us now write

$$\begin{aligned}\eta'_{\lambda_1}(s) &= a_0(\lambda) + a_1(\lambda)s + \cdots + a_n(\lambda)s^n, \\ \eta'_{\lambda_2}(s) &= b_0(\lambda) + b_1(\lambda)s + \cdots + b_n(\lambda)s^n.\end{aligned}$$

Since the coefficients of η'_{λ_1} and η'_{λ_2} are linear combinations of coefficients of η_{λ_1} and η_{λ_2} , respectively, it follows that $a_i(\lambda)$ and $b_i(\lambda)$ are continuous functions of λ . Since Λ is compact, these functions attain a maximum and a minimum. Assume $a_i(\lambda) \in [\alpha_i, \beta_i]$, $b_i(\lambda) \in [\gamma_i, \delta_i]$ for $\alpha_i \leq \beta_i$, $\gamma_i \leq \delta_i$, $i = 0, \dots, n$. Let us denote the columns of the $(2q+2) \times (n+q)$ matrix

$$(3.1.6) \quad \begin{bmatrix} \alpha_0 & \alpha_1 & \cdots & \alpha_n & & & & & & 0 \\ \gamma_0 & \gamma_1 & \cdots & \gamma_n & & & & & & \\ & \alpha_0 & \cdots & \alpha_{n-1} & \alpha_n & & & & & \\ & \gamma_0 & \cdots & \gamma_{n-1} & \gamma_n & & & & & \\ & & & \vdots & \vdots & & & & & \\ & & & \alpha_0 & \alpha_1 & \cdots & \alpha_n & & & \\ 0 & & & \gamma_0 & \gamma_1 & \cdots & \gamma_n & & & \end{bmatrix}$$

by $v_0^T, \dots, v_{n+q-1}^T$, respectively, and the columns of the above matrix (3.1.6) by α_i replaced with β_i , γ_i replaced with δ_i , $i = 0, \dots, n$, with $u_0^T, \dots, u_{n+q-1}^T$, respectively. Let us denote Δ'_1/Δ'_2 by

$$(3.1.7) \quad \Delta'_1/\Delta'_2(s) = \left[\sum_{i=0}^q c_i s^i \right] / \left[\sum_{i=0}^{q-1} d_i s^i + s^q \right]$$

where

$$(3.1.8) \quad \underline{\psi} \triangleq [c_0 \quad d_0 \quad \cdots \quad c_{q-1} \quad d_{q-1} \quad c_q \quad 1],$$

$$(3.1.9) \quad \underline{s}^T \triangleq [1, s, s^2, \dots, s^{n+q}]^T.$$

By Theorem 1.3 of [15] it follows that a sufficient condition for the family of polynomials $\Delta'_1 \eta'_{\lambda_2} - \Delta'_2 \eta'_{\lambda_1}$ for all $\lambda \in \Lambda - \{1, 2\}$ to be stable is given by the stability of the following four polynomials:

$$(3.1.10) \quad \begin{aligned}\alpha_1(s) &= \underline{\psi} [v_0^T v_1^T u_2^T u_3^T v_4^T \cdots] \underline{s}^T, \\ \alpha_2(s) &= \underline{\psi} [u_0^T u_1^T v_2^T v_3^T u_4^T \cdots] \underline{s}^T, \\ \alpha_3(s) &= \underline{\psi} [v_0^T u_1^T u_2^T v_3^T v_4^T \cdots] \underline{s}^T, \\ \alpha_4(s) &= \underline{\psi} [u_0^T v_1^T v_2^T u_3^T u_4^T v_4^T \cdots] \underline{s}^T.\end{aligned} \quad \square$$

Remark 3.1.5. The four polynomials in (3.1.10) have the same structure as we would obtain as return difference polynomials from four single-input single-output plants compensated by a stable, minimum phase compensator with the exception that the associated $(2q+2) \times (n+q)$ matrices in (3.1.10) are not the Sylvester matrices corresponding to any single-input single-output plants.

Remark 3.1.6. The proof of the above theorem relies on some recent results due to Kharitonov [28] (see [15] for details).

3.2. Simultaneous stabilization of one-parameter family of plants by interpolation methods. Let $x_1(s)/y_1(s)$ and $x_2(s)/y_2(s)$; $x_1, x_2, y_1, y_2 \in H$ be a pair of proper but not strictly proper plants in $\Omega_{1,1}''$ written in their coprime representation. For ease of exposition and notational simplicity we assume that the zeros of $x_1 y_2 - x_2 y_1(s)$ in \mathbb{C}_u

